

## PUBLISHED VERSION

Reppel, Julie-Ann; Alwahabi, Zeyad T..

Orthogonal planar laser polarization spectroscopy, *Applied Optics*, 2002; 41 (21):4267-4272.

Copyright © 2002 Optical Society of America

### PERMISSIONS

[http://www.opticsinfobase.org/submit/review/copyright\\_permissions.cfm#posting](http://www.opticsinfobase.org/submit/review/copyright_permissions.cfm#posting)

This paper was published in *Applied Optics* and is made available as an electronic reprint with the permission of OSA. The paper can be found at the following URL on the OSA website: <http://www.opticsinfobase.org/abstract.cfm?URI=ao-41-21-4267>. Systematic or multiple reproduction or distribution to multiple locations via electronic or other means is prohibited and is subject to penalties under law.

OSA grants to the Author(s) (or their employers, in the case of works made for hire) the following rights:

(b) The right to post and update his or her Work on any internet site (other than the Author(s)' personal web home page) provided that the following conditions are met: (i) access to the server does not depend on payment for access, subscription or membership fees; and (ii) any such posting made or updated after acceptance of the Work for publication includes and prominently displays the correct bibliographic data and an OSA copyright notice (e.g. "© 2009 The Optical Society").

17<sup>th</sup> December 2010

<http://hdl.handle.net/2440/761>

# Orthogonal planar laser polarization spectroscopy

Julie Reppel and Zeyad T. Alwahabi

Planar laser polarization spectroscopy has recently been used to image the hydroxyl radical in combustion for small intersection angles of pump and probe beams. We report an experimental configuration that allows planar laser polarization imaging for perpendicular intersection of pump and probe beams. We demonstrate what to our knowledge is the first planar laser polarization spectroscopy imaging at a 90° intersection of pump and probe beams for both linearly and circularly polarized pump beams. © 2002 Optical Society of America

OCIS codes: 120.0120, 120.1740.

## 1. Introduction

Polarization spectroscopy is based on detection of the induced polarization change in a weak probe beam that is due to the passage of a strong pump laser beam through an optically thin medium. A strong linearly or circularly polarized pump beam is used to create population anisotropy of Zeeman sublevels. A weak linearly polarized probe beam that crosses the pump beam path experiences linear birefringence and dichroism that are due to the Zeeman population anisotropy if the probe polarization direction contains components that are parallel and perpendicular to the pump beam polarization. The signal strength is maximized if the probe beam polarization is equally divided between parallel and perpendicular components. For a circularly polarized pump beam, the linearly polarized probe beam undergoes circular dichroism and birefringence. The weak polarization signal is detected by placement of crossed polarizers in the probe beam path that enclose the pump-probe beam intersection volume.

Conventionally, polarization spectroscopy is implemented in a counterpropagating, Doppler-free<sup>1</sup> pump and probe beam geometry to maximize signal strength. However, polarization spectroscopy imaging requires a finite beam intersection angle.

Polarization spectroscopy imaging of the hydroxyl radical in a premixed CH<sub>4</sub>/O<sub>2</sub> flame for pump-probe beam intersection angles of 15° and 30° has been demonstrated by Nyholm *et al.*<sup>2</sup> The linearly polarized probe beam intersected a horizontally polarized pump laser sheet, and the probe beam was polarized at 45° to the vertical. The OH distribution within the elliptical interaction region was imaged on the circular cross section of the pump beam. The signal strength was shown experimentally to follow a cot<sup>2</sup>(θ) dependence on the intersection angle of pump and probe beams θ. A cot<sup>2</sup>(θ) dependence of polarization spectroscopy signal strength in the weak saturation regime was previously noted by Zizak *et al.*<sup>3</sup> for the case of a circularly polarized pump beam. The Zizak *et al.* experiment was limited to pump-probe beam intersection angles of less than 30° owing to weak signal strength. Zizak *et al.*<sup>3</sup> and Nyholm *et al.*<sup>2</sup> explained the cot<sup>2</sup>(θ) dependence in terms of the combined effects of the change in the interaction volume between pump and probe beams and the projection of the pump beam polarization on that of the probe beam.

The reported cot<sup>2</sup>(θ) falloff in signal strength with increasing intersection angle leads to a zero signal strength for a pump-probe beam intersection angle of 45°. In imaging applications, the decreased signal strength must be matched against increased horizontal resolution of the imaged elliptical cross section. Here we report an experimental configuration based on recent theoretical results<sup>4</sup> that leads to a nonzero signal at a 90° pump-probe intersection angle. The configuration can relax the small intersection angle requirement for polarization spectroscopy imaging.

---

J. Reppel and Z. T. Alwahabi (zalwahab@chemeng.adelaide.edu.au) are with the Department of Chemical Engineering, Adelaide University, Adelaide, S.A. 5005, Australia. J. Reppel is also with the Department of Mechanical Engineering.

Received 8 June 2001; revised manuscript received 3 March 2002.

0003-6935/02/214267-06\$15.00/0

© 2002 Optical Society of America

## 2. Theory

For perfectly crossed probe beam polarizers, the polarization spectroscopy signal is given by<sup>5</sup>

$$I = I_{\text{probe}} \left[ \xi + \frac{1}{16} (\Delta\alpha L)^2 L(x) \right], \quad (1)$$

where  $I$  is the detected intensity,  $I_{\text{probe}}$  is the input probe beam intensity,  $\xi$  represents the extinction ratio of the probe beam polarizers,  $\Delta\alpha$  is the induced dichroism,  $L$  is the interaction distance of pump and probe beams measured along the probe beam path,  $L(x)$  represents the line-shape function, recently calculated by Reichardt and Lucht<sup>6</sup> to be Lorentzian cubed in the low saturation regime, and  $x$  is the detuning from resonance.

The geometric dependence of the polarization spectroscopy signal strength lies in the terms  $\Delta\alpha$  and  $L$ . The pump–probe interaction length  $L$  is given by

$$L = W/\sin(\theta), \quad (2)$$

where  $W$  is the width of the pump sheet, which contributes a  $\csc^2(\theta)$  factor to the overall signal dependence.

The induced dichroism  $\Delta\alpha$  is related to the induced birefringence  $\Delta n$  by the Kramers–Kronig relations. Reppel and Alwahabi<sup>4</sup> derived an expression for the geometric dependence of the induced linear birefringence for the case of a linearly polarized pump beam by proposing that the optical properties of the pumped region be analogous to the birefringent properties of a uniaxial crystal. An equivalent expression for the induced circular birefringence in the case of a circularly polarized pump beam was derived by analogy with the optical properties of an optically active uniaxial crystal.

The ordinary refractive index,  $n_o$ , is independent of the direction of propagation. In a uniaxial crystal, however, the effective extraordinary refractive index,  $n(\theta)_e$ , is a function of the angle of propagation from optic axis  $\theta$ . The magnitude of the effective birefringence,  $|\Delta n(\theta)| = |n(\theta)_e - n_o|$ , oscillates between a maximum value,  $\Delta n_{\text{max}} = |n_e - n_o|$ , for propagation normal to the optic axis and zero for propagation along the optic axis.

For polarization spectroscopy, the induced optic axis can be defined as the polarization direction of the pump beam. Assuming that the induced birefringence is small, Reppel and Alwahabi<sup>4</sup> showed that the linear birefringence induced by a linearly polarized pump beam is

$$n(\theta)_e - n_o = \sin^2(\varphi)(n_e - n_o), \quad (3)$$

where  $\varphi$  is the angle between the direction of propagation of the probe beam and the induced optic axis

(corresponding to the polarization direction of the pump beam). It can easily be seen that, for pump and probe beams intersecting in the horizontal plane at angle  $\theta$ , a horizontally polarized pump beam leads to a  $\cos^2(\theta)$  dependence of the induced birefringence. The resultant polarization spectroscopy signal strength  $I$ , when the pump beam is horizontally polarized, is

$$I = I_{\text{probe}} \left\{ \xi + \frac{1}{16} \left[ \frac{\cos^2(\theta)}{\sin^2(\theta)} \right] \Delta\alpha_{\text{max(linear)}}^2 L^2 L(x) \right\}, \quad (4)$$

which follows the  $\cot^2(\theta)$  dependence reported by Nyholm *et al.*<sup>2</sup> The term  $\Delta\alpha_{\text{max(linear)}}$  is the maximum induced dichroism for collinear pump and probe beams. This dichroism was evaluated by Teets *et al.*<sup>5</sup> by means of summation, over the Zeeman states of the lower level of the probe beam transition, of functions of the Clebsch–Gordon coefficients. The dichroism is related to the maximum induced birefringence  $\Delta n_{\text{max(linear)}}$  by the Kramers–Kronig relations.

A vertically polarized pump beam, however, induces a linear birefringence that is independent of the intersection angle of pump and probe beams. The polarization spectroscopy signal strength for a vertically polarized pump beam then follows a  $\csc^2(\theta)$  dependence on pump–probe beam intersection angle

$$I = I_{\text{probe}} \left\{ \xi + \frac{1}{16} \left[ \frac{1}{\sin^2(\theta)} \right] \Delta\alpha_{\text{max(linear)}}^2 L^2 L(x) \right\}. \quad (5)$$

Note that Eqs. (4) and (5) assume that the probe beam is polarized at  $45^\circ$  to the pump beam polarization axis.

Reppel and Alwahabi<sup>4</sup> derived a general expression for the linear dichroism induced by a linearly polarized pump beam by considering pump and probe beams intersecting at angle  $\theta$  in a horizontal plane. The pump beam was polarized at angle  $\kappa$ , and the probe beam was polarized at angle  $\gamma$  to the vertical. In each case, the vertical axis and the direction of propagation of the beam represent the  $X$  and  $Z$  axes, respectively, of a right-handed system to define the positive direction of rotation of angles  $\kappa$  and  $\gamma$ . The polarization spectroscopy signal strength  $I$  for a linearly polarized pump beam is written as

$$I = I_{\text{probe}} \left[ \xi + \frac{1}{16} F(\gamma, \kappa, \theta)_{\text{lin}} \Delta\alpha_{\text{max(linear)}}^2 L^2 L(x) \right], \quad (6)$$

where the geometric dependence is contained in the factor  $F(\gamma, \kappa, \theta)_{\text{lin}}$ :

$$F(\gamma, \kappa, \theta)_{\text{lin}} = \frac{1}{\sin^2(\theta)} \frac{\{\sin(2\gamma)[\cos^2(\kappa) - \sin^2(\kappa)\cos^2(\theta)] - \cos(2\gamma)\sin(2\kappa)\cos(\theta)\}^2}{[1 - \sin^2(\kappa)\sin^2(\theta)]}. \quad (7)$$

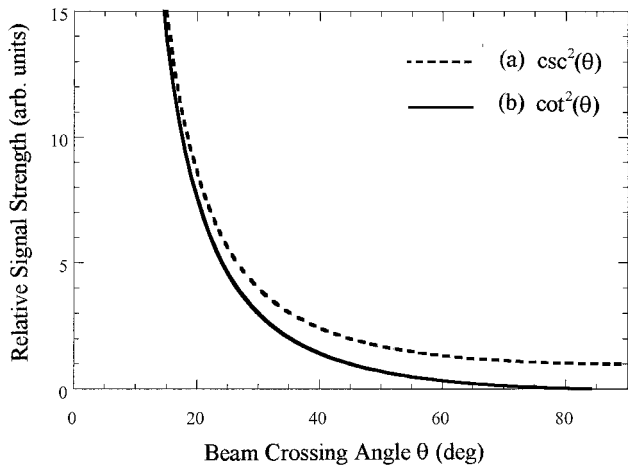


Fig. 1. Dependence of polarization spectroscopy signal strength on pump-probe beam intersection angle  $\theta$  for a pump beam polarized (a) in the plane of intersection and (b) normal to the plane of intersection.

For copropagating and counterpropagating pump beams, Eq. (7) reduces to

$$F(\gamma, \kappa, 0)_{\text{lin}} = \frac{\sin^2[2(\gamma - \kappa)]}{\sin^2(\theta)}, \quad (8)$$

$$F(\gamma, \kappa, \pi)_{\text{lin}} = \frac{\sin^2[2(\gamma + \kappa)]}{\sin^2(\theta)}, \quad (9)$$

respectively. For a horizontally polarized pump beam and a probe beam polarized at  $45^\circ$  to the vertical, Eq. (7) reduces to the  $\cot^2(\theta)$  dependence noted in Eq. (4). Similarly, for a vertically polarized pump beam and a probe beam polarized at  $45^\circ$  to the vertical, the equation reduces to the  $\csc^2(\theta)$  dependence of Eq. (5).

These two functions are plotted in Fig. 1. The  $\cot^2(\theta)$  function drops to zero signal for a  $90^\circ$  intersection of pump and probe beams, whereas the  $\csc^2(\theta)$  function exhibits nonzero signal strength for a  $90^\circ$  pump-probe intersection. The  $\csc^2(\theta)$  signal decreases rapidly with an increased intersection angle. However, for the purpose of imaging, pump-probe intersection at  $90^\circ$  is desirable. The gain in resolution at the orthogonal intersection of pump and probe beams is optimized against the decreased signal strength at the large pump-probe beam intersection angles. If we assume that a minimum intersection angle of  $10^\circ$  is required for effective imaging, the ratio of signal strengths for imaging at  $10^\circ$  and  $90^\circ$  is 33:1. However, the ratio of signal strengths drops by only a factor of 4 for polarization spectroscopy imaging between the pump-probe intersection angles of  $30^\circ$  and  $90^\circ$ .

The Reppel and Alwahabi<sup>4</sup> expressions for geometric dependence,  $F(\gamma, \theta)_{\text{lin}}$ , of the polarization spectroscopy signal strength for a circularly polarized pump beam are based on an approximate expression for the induced birefringence between two polarization

modes of propagation for the optically active uniaxial crystal,  $\alpha$  and  $\beta$ :

$$n(\theta)_\alpha - n(\theta)_\beta = n_o \left[ \sin^4(\theta) \left( \frac{\Delta + \sigma^2}{2} \right)^2 + \cos^2(\theta) \sigma^2 \right]^{1/2}. \quad (10)$$

The terms  $\Delta/2$  and  $\sigma$  are identified as the maximum induced linear dichroism and the maximum induced circular dichroism, respectively, and were calculated by Teets *et al.*<sup>5</sup>

The expressions for geometric dependence of the polarization spectroscopy signal strength are based on two regions of approximation. For probe beam propagation close to the optic axis, defined as the polarization axis of the circularly polarized pump beam, the induced birefringence is approximated by

$$n(\theta)_\alpha - n(\theta)_\beta = \cos(\theta) \sigma n_o. \quad (11)$$

For probe beam propagation near normal to the optic axis,

$$n(\theta)_\alpha - n(\theta)_\beta = \sin^2(\theta) \frac{(\Delta + \sigma^2)}{2} n_o. \quad (12)$$

The geometric dependences of the signal strength for these two regions of interest are

$$F(\gamma, \theta)_{\text{circ}(\theta=0)} = \frac{1}{\sin^2(\theta) \cos^2(\theta)} \times \left\{ \begin{aligned} & [\cos^2(\gamma) \sin^4(\theta) \Delta + \cos^2(\theta) \sigma^2]^2 \\ & + \frac{1}{4} [\cos(\theta) \sin^2(\theta) \sin(2\gamma) (\Delta - \sigma^2)]^2 \end{aligned} \right\} \quad (13)$$

for  $\cos^2(\theta) \ll \sigma^2, \Delta$ , and

$$F(\gamma, \theta)_{\text{circ}[\theta \sim (\pi/2)]} = \sin^2(2\gamma) \sin^2(\theta) \left( \frac{\Delta + \sigma^2}{2} \right)^2 \quad (14)$$

for  $\cos^2(\theta) \gg \sigma^2, \Delta$ . Note that, for Eqs. (13) and (14), the maximum induced linear and circular dichroisms have been included in the geometric dependence of the polarization spectroscopy signal strength.

The polarization axis of the circularly polarized pump beam lies parallel to the direction of propagation. For pump and probe beams that intersect at angle  $\theta$  in the horizontal plane and a probe beam polarized in the horizontal plane, Eq. (13) reduces to

$$F\left(\frac{\pi}{2}, \theta\right)_{\text{circ}(\theta=0)} = \cot^2(\theta) \sigma^2, \quad (15)$$

indicating a rapid falloff in signal strength with an increased angle of the pump-probe intersection. However, for normal incidence of pump and probe beams and an unspecified probe beam polarization direction, Eq. (14) can be rewritten as

$$F\left(\gamma, \frac{\pi}{2}\right)_{\text{circ}[\theta \sim (\pi/2)]} = \sin^2(2\gamma) \left( \frac{\Delta + \sigma^2}{2} \right)^2, \quad (16)$$



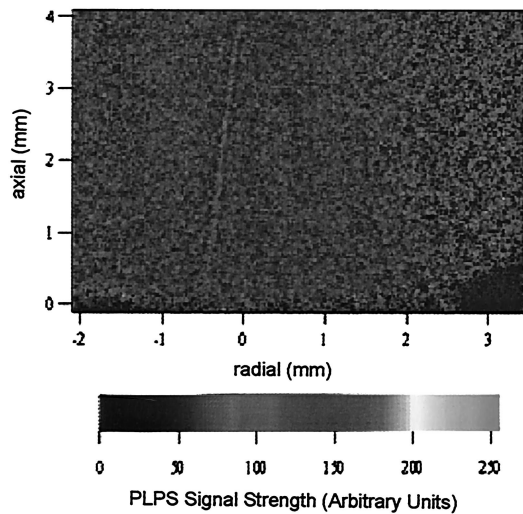


Fig. 5. Average OH [ $A^2\Sigma-X^2\Pi(0-0) Q_2(8)$  transition] orthogonal PLPS signal in a laminar premixed  $\text{CH}_4/\text{O}_2$  flame produced by a 1-mm jet exit diameter burner ( $\text{Re} \sim 3050$ ). The pump beam is horizontally polarized and the probe beam is polarized at  $45^\circ$  from the vertical. The lack of signal supports the  $\cot^2(\theta)$  dependence of signal strength for this polarization configuration noted by Nyholm *et al.*<sup>2</sup>

intersection of pump and probe beams for linearly and circularly polarized pump beams, respectively. The linearly polarized pump beam is vertical, i.e., polarized normal to the plane of intersection of the pump and probe beams. The images are 50 shot averages. The tip of the burner can be seen at the base of each image. The images have been corrected for the average probe beam profile.

Figure 5 shows the equivalent orthogonal PLPS average image for a linearly polarized pump beam polarized horizontally, i.e., polarized in the plane of intersection of the pump and probe beams. The lack of signal corresponds to the zero signal strength predicted for normal pump-probe beam intersection by Eq. (7) and the  $\cot^2(\theta)$  dependence noted by Nyholm *et al.*<sup>2</sup>

The instantaneous images do not differ from the average images, owing to flame stability. Figures 6 and 7 show the image quality of an instantaneous image for a linearly polarized pump beam polarized vertically and for a circularly polarized pump beam, respectively. Maximum instantaneous signal-to-background ratios of 34:1 for a linearly polarized pump beam indicate that a signal-to-background ratio of 1100:1 is possible for an intersection angle of  $10^\circ$  with this polarization configuration. The maximum instantaneous signal-to-background ratios detected for the circularly polarized pump beam were 43:1.

The images do not require elongation in the horizontal direction, as is the case for small intersection angle polarization spectroscopy. The imaged region is  $\sim 5$ – $6$  mm wide and 4 mm high. The image resolution is  $9.5 \mu\text{m}/\text{pixel}$  for both linearly and circularly polarized pump beams. The thickness of the

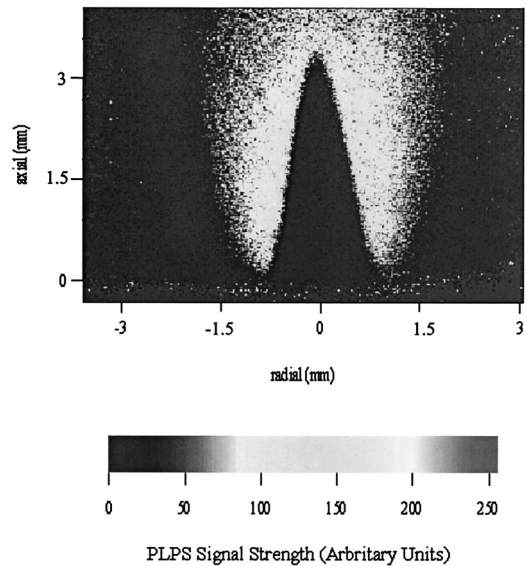


Fig. 6. Instantaneous OH [ $A^2\Sigma-X^2\Pi(0-0) Q_2(8)$  transition] orthogonal PLPS signal for the laminar premixed  $\text{CH}_4/\text{O}_2$  flame imaged in Fig. 3. The pump beam is vertically polarized and the probe beam is polarized at  $45^\circ$  from the vertical.

elliptical interaction region was estimated to be  $700 \mu\text{m}$ .

#### 4. Conclusions

We have demonstrated that planar laser polarization spectroscopy is possible for perpendicular pump-probe beam intersection for both linearly and circularly polarized pump beams. Both instantaneous and average orthogonal PLPS images have been pre-

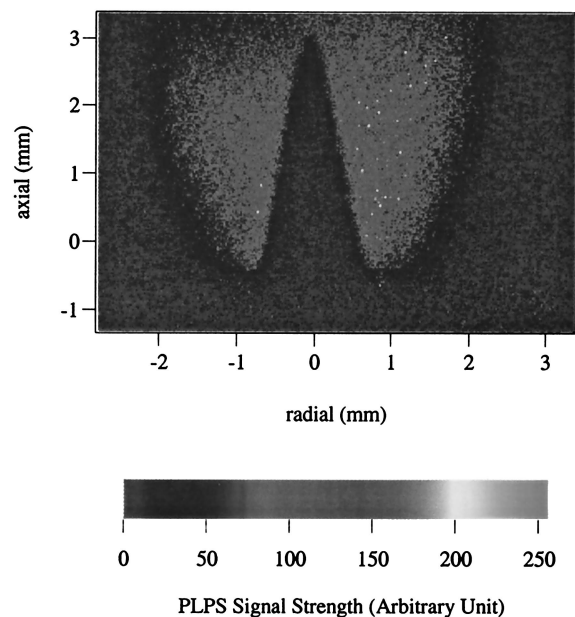


Fig. 7. Instantaneous OH [ $A^2\Sigma-X^2\Pi(0-0) Q_2(8)$  transition] orthogonal PLPS signal for the laminar premixed  $\text{CH}_4/\text{O}_2$  flame imaged in Fig. 4. The pump beam is circularly polarized and the probe beam is polarized at  $45^\circ$  from the vertical.

sented. For maximum signal strength, the polarization direction of the linearly polarized pump beam should be normal to the plane of intersection of the pump and probe beams and the probe beam polarization should be  $45^\circ$  from that of the pump beam.

The orthogonal PLPS imaging method does not require elongation of the collected image to represent the imaged area, maximizing spatial resolution at the expense of signal strength. However, the small pump-probe beam intersection angle required for significant increases in the signal strength for non-orthogonal PLPS (an increase by a factor of 4 for imaging at  $30^\circ$  pump-probe beam intersection angle and an increase by a factor of 33 for imaging at  $10^\circ$  intersection angle) leads to a significant decrease in the spatial resolution of the technique. Small-angle PLPS is also dependent on the quality of the probe beam profile in the intersection region of pump and probe beams because any imperfection is emphasized by the required stretching of the collected image to represent the elliptical interaction region.

This research was supported by the Australian Research Council.

## References

1. C. Wieman and T. W. Hänsch, "Doppler-free laser polarization spectroscopy," *Phys. Rev. Lett.* **36**, 1170–1173 (1976).
2. K. Nyholm, R. Fritzon, and M. Alden, "Two-dimensional imaging of OH in flames by use of polarization spectroscopy," *Opt. Lett.* **18**, 1672–1674 (1993).
3. G. Zizak, J. Lanauze, and J. D. Winefordner, "Cross-beam polarization in flames with a pulsed dye laser," *Appl. Opt.* **25**, 3242–3246 (1986).
4. J. Reppel and Z. T. Alwahabi, "A uniaxial gas model of the geometrical dependence of polarization spectroscopy," *J. Phys. D* **34**, 2670–2678 (2001).
5. R. E. Teets, F. V. Kowalski, W. T. Hill, N. Carlson, and T. W. Hänsch, SPIE, "Laser Polarisation Spectroscopy," in *Advances in Laser Spectroscopy I*, A. H. Zewail, ed., *Proc. SPIE* **113**, 80–87 (1977).
6. T. A. Reichardt and R. P. Lucht, "Theoretical calculation of line shapes and saturation effects in polarization spectroscopy," *J. Chem. Phys.* **109**, 5830–5843 (1998).